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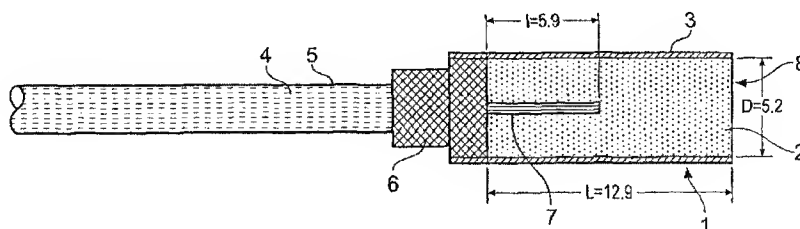
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For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

(54) Title: MICROWAVE APPLICATOR



(57) Abstract: A microwave applicator comprising a coaxial electrical input (4) and a waveguide (1) filled with dielectric (2), an inner conductor (7) of the coaxial input extending longitudinally within one end of the waveguide to launch microwaves in the TM₀₁ mode to travel to the distal end face (8) of the waveguide so that microwaves are transmitted when the distal end face is contacted by the biological tissue to be treated.

MICROWAVE APPLICATOR

Technical Field

This invention relates to a microwave applicator suitable for heating biological tissue and a method of heat treating surface tissue.

The applicants have previously proposed a microwave applicator for surgical use comprising a waveguide of reduced diameter by virtue of containing a dielectric of high permittivity. A coaxial electrical input generates microwaves in the TE_{11} mode within the dielectric and these radiate from the distal end face of the waveguide.

Disclosure of the Invention

According to a first aspect, the present invention, consists in a microwave applicator comprising a coaxial electrical input and a waveguide filled with dielectric, a central conductor of the coaxial input extending longitudinally within one end of the waveguide to launch microwaves preferably in the TM_{01} mode, to travel to the distal end face of the waveguide so that microwaves are transmitted from the distal end face when in contact with the biological tissue to be treated.

The TM_{01} mode is preferred because it has a field pattern that is a good match with the coaxial input, better than the fundamental TE_{11} mode more commonly used. The TM_{01} also produces a simple transition between the coaxial input and the waveguide. The central conductor is preferably coaxially aligned within a circular waveguide and extends a short way within the waveguide to match the general dimensions of the waveguide, especially its length and diameter, and the permittivity of the dielectric and frequency of the electrical input.

The distal end face of the waveguide is preferably flat and radiates microwave energy with parallel wavefronts that advance into the biological tissue in contact with the distal end face and have minimum lateral spreading. The depth of penetration of the microwaves is dependent upon the frequency and electrical input power, but typically only a small distance of penetration is required for local heat treatment of tissue in microsurgery. In an

alternative embodiment, the distal end face may be slightly domed and centred on the axis of the waveguide instead of being flat.

Another particularly important feature of the invention is the ability to make use of resonance in the waveguide so that reflections from the transition at the input end, and from the distal end face caused by the change in dielectric at each, are out of phase and therefore enhance forwards transmission when the distal end face is in contact with the biological tissue, and are in phase and therefore enhance reflection to the coaxial input when the distal end face is out of contact with the biological tissue. Therefore, microwave energy is only transmitted to any appreciable extent from the distal end face when in contact with the biological tissue to be treated, and this is a key safety feature in the mode of operation.

According to a second aspect, the invention consists in a microwave applicator comprising a waveguide, a coaxial electrical input with a central conductor extending longitudinally within one end of the waveguide to launch microwaves preferably in the TM_{01} mode, that travel to the distal end of the waveguide and are transmitted into biological tissue to be treated, a diaphragm of low loss dielectric material being provided within the waveguide so as to extend laterally of the waveguide to reflect the microwaves travelling along it, the longitudinal location of the diaphragm being selected in relation to the ends of the waveguide so that the coherent addition of the reflected waves from the waveguide junction and the diaphragm combine to create a wave which is of correct magnitude and phase to cancel the reflection from the coaxial waveguide junction.

Preferably, the thickness of the diaphragm and the permittivity of the dielectric material from which the diaphragm is made are selected to determine the magnitude of the rearward reflection of microwaves from the diaphragm for optimum cancellation of the rearward reflection in the coaxial input.

Preferably, the waveguide is air-filled, and the distal end of the waveguide is adapted to contact (or nearly contact) the surface tissue to be treated.

The microwave applicator of the first or second aspect of the invention can be used in a method of heat treating surface tissue, the distal end face of the waveguide being brought into contact with the surface tissue for treatment.

Description of the Drawings

The invention will now be described by way of example with reference to the accompanying drawings, in which:

Figure 1 is an axial section of a flexible laparoscopic microwave applicator according to a first embodiment of the invention;

Figure 2 shows graphs of reflection coefficient against microwave frequency for the applicator of Figure 1 when the distal end is in air (graph S) and when in contact with biological tissue (graph T);

Figure 3 is an axial section of a microwave applicator according to a second embodiment of the invention;

Figure 4 is an axial section of a microwave applicator according to a third embodiment of the invention;

Figure 5 is an axial section of a microwave applicator according to a fourth embodiment of the invention;

Figure 6 is an axial section of a microwave applicator according to a fifth embodiment of the invention; and

Figure 7 is a schematic drawing of a microwave applicator in use for medical treatment according to the invention.

Embodiments of the Invention

The microwave applicator of Figure 1 consists of a waveguide 1 formed by a cylindrical body of dielectric 2 covered in an outer layer of aluminium foil 3, and a flexible coaxial cable input power supply 4 which is connected to the waveguide at one end so that the

outer conductor 5 of the coaxial cable is electrically connected via a copper ferrule 6 to the aluminium tape 3, and the inner conductor 7 of the coaxial cable extends axially a short distance l into the dielectric body 2. The distal end face 8 of the waveguide 1 is flat and is covered by a layer of a non-stick polymer coating such as FEP or paralene.

The waveguide 1 preferably operates in the TM_{01} mode.

Typically, for this microwave applicator to operate at a frequency of 9.2 GHz the dimensions of the waveguide are as follows; overall length $L = 12.9$ mm, diameter $D = 5.2$ mm, $l = 5.9$ mm; and the permittivity of the dielectric body $k = 25$. The dielectric is typically, Hik 500f dielectric material sold by Emerson & Cummings.

The performance of the microwave applicator of Figure 1 at different frequencies is shown by the graphs of Figure 2, in which Graph S shows the variation of reflection coefficient S_{11} when the distal end face 8 of the applicator is in air, and in which Graph T shows the variation of reflection coefficient S_{11} when the distal end face 8 of the applicator is in contact with biological tissue to be treated. A drop in value of S_{11} in Figure 2 is indicative of a good microwave match, which is clearly demonstrated in Graph T at the designed operating frequency of 9.2GHz. Under these conditions, the applicator is transmitting maximum microwave energy into the biological tissue, but if the contact with the tissue is broken and the distal end face is in air or gas such as CO_2 , then the transmitted energy falls immediately to a much lower level as the energy is reflected back to the coaxial cable input power supply 4.

It will be appreciated that a microwave applicator as shown in Figure 1 can be relatively inexpensive to manufacture, and can therefore be sold as a disposable product for microsurgery.

The microwave applicator of Figure 1, being of reduced diameter of 5.2 mm, is suitable for insertion through a Trocar in laproscopic surgery to produce a local heating effect in a controlled manner adjacent the distal end face when in contact with biological material.

For example, such an applicator may be used to destroy small surface tumours, for the treatment of ovarian cancer, or the treatment of endometriosis, or any surface lesions.

The second embodiment of the invention shown in Figure 3 is similar in configuration to that of Figure 1, and the same reference numbers are used for equivalent components. However, the waveguide 1 comprises a rigid aluminium cylindrical wall 13, typically 2 mm thick, and the dielectric body 2 is composed of a hard ceramic material, such as stabilised zirconia (TECHNOX[®] 2000) which has a permittivity $K = 25$. This dielectric material gives the applicator an ability to handle higher power levels, typically, up to 200 watts, compared with a power level of, say, 45 watts for the applicator of Figure 1. The waveguide 1 preferably operates in the TM_{01} mode.

The applicator of Figure 3 is designed to operate at a lower frequency of 2.45 GHz, and also has an increased length $L = 50$ mm and diameter $D = 20$ mm. It will be appreciated that the diameter D is determined by the frequency of operation and permittivity K , and is selected to allow treatment of an appropriate size area of tissue, the increased area compared with Figure 1 being balanced by the increased power to provide an appropriate power density at the distal end 8 for the treatment intended.

The projection l of the central conductor 7 extends 25 mm into the dielectric body 2, and an air gap 9 is provided between the outer conductor 5 and dielectric of the coaxial cable input 4 and the waveguide 1 to allow the dielectric filling of the coaxial cable to expand.

The applicator of Figure 3 with a larger distal end 8 is more suitable for the treatment of larger surface breaking tumours, for example, primary and secondary tumours on the liver.

In an alternative embodiment of the invention, suitable for treating smaller liver tumours, the same configuration as that of Figure 3 is used but, the stabilised zirconia dielectric is replaced by alumina having a permittivity $K = 10$, and the dimensions are as follows: $L = 18$ mm; $D = 10$ mm; $l = 11$ mm; and the operating frequency is 9.2 GHz. This applicator will treat a small area of tissue than that of Figure 3, but will cause less collateral damage.

The microwave applicator shown in Figure 4 consists of an air-filled waveguide 11 formed by an aluminium cylindrical wall 13 with an input connection 14 for a flexible coaxial cable input power supply which is connected to the waveguide at one end. The outer surface of the wall 13 is covered by a UPVC sleeve 16. The outer conductor of the coaxial cable is electrically connected to the wall 13 of the waveguide via a brass fitting 17, and the inner conductor of the coaxial cable is connected to a conductor 15 which extends axially a short distance l into the waveguide 11. A PTFE bush 18 separates and forms an electrical insulator between the conductor 15 and fitting 17. A Perspex diaphragm 20 is located laterally within the waveguide near the open end within a rebated section 21 which spaces it a distance w away from the open end 18. The diaphragm 20 has a thickness t . The waveguide 11 preferably operates in the TM_{01} mode.

The operating frequency of the applicator is 7 GHz and the dimensions are typically $L = 108\text{mm}$; $D = 42\text{mm}$; $l = 13\text{mm}$; $w = 27.7\text{mm}$; and $t = 4.3\text{mm}$. These dimensions are selected in connection with the operating frequency and permittivity of the diaphragm so that when in use with the open end of the waveguide in contact with surface tissue to be treated, the rearward reflections of microwaves from the tissue and the transition between the coaxial cable 14 and waveguide 11 are substantially cancelled out by the reflections from the diaphragm which reduces reflections within the coaxial cable. In this balance situation, the majority of the microwave energy is then transmitted to the tissue being treated. In particular, the thickness t of the diaphragm 20 and the permittivity k of the material of which it is composed will determine the size of rearward reflection of microwaves from it. The location of the diaphragm 20 relative to the ends of the waveguide 11 will determine the relative phases of the rearward reflections of the microwaves.

A microwave applicator such as that of Figure 4 would be suitable for skin treatments such as the treatment of psoriasis, especially because the end of the probe has minimal contact with the tissue being treated. Preferably, the edge of the waveguide 11 at the open end may be coated or fitted with some other protection (22) such as silicone rubber, for engagement with the tissue.

An alternative embodiment of the invention is illustrated in Figure 5 in which the microwave applicator consists of a waveguide 31 supported at one end of a rigid tube 32 having a handle 33 and input power connection 34 at its other end. The applicator is held and manipulated by the handle 33 and the waveguide 31 forms a treatment head. A coaxial cable 35 extends through the tube 32 and connects the input power connection 34 to the waveguide 31.

The waveguide 31 consists of a cylindrical aluminium sleeve 36 which is connected to an aluminium end cap 37 at the input end. An aluminium support bush 38 is connected at one end to a central bore 39 in the end cap 37, and is connected at its other end to the tube 32 so that the coaxial cable 35 can pass through it. The outer conductor 40 of the coaxial cable 35 is exposed and electrically connected to the end cap 37, and the inner conductor 41 of the coaxial cable 35 is exposed to project axially into the waveguide 31. A cylindrical body 42 of dielectric comprising TECHNOX® 2000 ceramic is fitted within the sleeve 36 and is formed with a central bore 43 to receive the inner conductor 41. An air gap 44 is formed between the end of the dielectric filling 45 of the coaxial cable and the dielectric body 42 of the waveguide.

The handle 33 is machined from aluminium and has a concentric recess 45 at its input end to receive the input power connection 34. A central bore 46 in the handle accommodates the coaxial cable 35.

The waveguide 31 preferably operates in the TM_{01} mode.

Typically, the applicator is designed to operate at 2.45 GHz and the dimensions of the waveguide comprise a sleeve 36 of length $L = 50$ mm and inner diameter $D = 20$ mm, and an inner conductor 41 with an exposed length $l = 11.8$ mm and an air gap 44 of length 2 mm. The tube 32 is typically stainless steel and has a diameter of 8 mm and length 250 mm or other appropriate length to reach tissue being treated. The tube 32 may be bent laterally at one or more locations 46 along its length to improve the ease with which the radiation emitting end face 47 of the treatment head can be engaged in surface-to-surface contact with tissue to be treated..

Another embodiment of the invention is illustrated in Figure 6, which like that of Figure 5, consists of a waveguide 51 forming a treatment head at one end of a rigid tube 52, and a handle and input power connection (not shown) at the other end of the tube 52. The waveguide 51 consists of a machined aluminium component consisting of a cylindrical sleeve 54 and end wall 55 having an aperture 56 to receive the tube 52 and coaxial cable 57. A cylindrical body of dielectric 58 comprising Hik500f is fitted inside the sleeve 54 and is formed with a central bore 59 to receive the inner conductor 60 of the coaxial cable 57. The outer conductor 61 of the cable 57 is electrically connected to the end wall 55 and an air gap 62 is formed between the end of the dielectric filling 63 of the cable 57 and the dielectric body 58.

Typically, the applicator is designed to operate at 9.2 GHz and the waveguide dimensions comprise a sleeve 54 of length $L = 16$ mm and inner diameter 10 mm, and an inner conductor 60 with an exposed length of 13 mm, and an air gap 62 of 2 mm.

The microwave applicator of Figures 5 and 6 can be used, like the applicators of Figures 1 and 3, to treat tumours or other surface lesions, or for the treatment of endometriosis. The treatment head is inserted through an opening in a patient's body, either through a Trocar or directly through a larger incision. The applicator is then manipulated to bring the end face of the treatment head into face-to-face contact with the tissue to be treated adjacent the tumour or lesion. Microwave radiation emitted from the end face of the treatment head is then transmitted into the tumour or lesion and surrounding tissue and causes it to be ablated. This process can be repeated as necessary to ablate multiple tumours or lesions at different locations before the treatment is completed.

A microwave applicator according to the invention can also be used to stop the flow of blood from bleeding tissue by bringing the end face of the treatment head into contact with the bleeding tissue and transmitting radiation to ablate the tissue.

Although the methods of medical treatment described above use the microwave applicators illustrated it should be appreciated that the invention also relates generally to the method of treating tumours or lesions on or within the surface of tissue, especially the liver, using any form of microwave applicator having a treatment head with a radiation emitting surface

which can engage the tissue in face-to-face contact so as to transmit radiation into the tissue.

Figure 7 illustrates medical treatment of surface tumours on a patient's liver 70. An incision is made across the patient's abdomen and the abdominal wall is held in clamps 71 to create an opening into the abdominal cavity. The liver is then freed from the surrounding tissue so that it can be accessed for treatment. The condition of the liver is assessed and decisions are made as to the treatment to be given, whether to remove part of the liver and/or to ablate part of the liver. In the drawing, the liver shown has multiple surface tumours 72 which require ablation. A microwave applicator 73, preferably such as illustrated in any of Figures 1 to 6, is manipulated to align the end face of the treatment head with a tumour, and to bring the end face into contact with the tumour. The power supply to the applicator is then switched on so that it generates microwaves that irradiate the tumour, causing it to be ablated. The applicator is then lifted away from the liver surface either before or after the power has been reduced or switched-off. The whole process is then repeated multiple times to ablate each of the surface tumours in turn.

Real time intra-operative ultrasound scanning is used to assess the location and extent of the tumours within or on the surface of the liver. Also, the extent of the ablation achieved when treating an individual tumour is assessed using intra-operative ultrasound scanning. The ablated tissue appears as a "thermal cloud" emanating from the end face of the applicator when viewed in the scan output. The treatment is therefore continued until the "thermal cloud" encompasses the whole of the tumour and a safety margin around it.

A larger tumour or tumours may require removal of part of the liver. This is done by cutting the liver, which causes bleeding. The microwave applicator is then used to stem the bleeding by bringing the end face of the treatment head into contact with the bleeding surface and turning on the power to the applicator to ablate the bleeding surface. This procedure is then repeated over the whole of the bleeding surface.

Once treatment of the liver is completed, the abdomen is washed with saline solution, and the abdominal wall is sutured.

CLAIMS

1. A microwave applicator comprising a coaxial electrical input (4) and a waveguide (1) filled with dielectric (2), an inner conductor (7) of the coaxial input (4) extending longitudinally within one end of the waveguide (1) to launch microwaves mode to travel to the distal end face (8) of the waveguide (1) so that microwaves are transmitted when the distal end face (8) is contacted by biological tissue to be treated.
2. A microwave applicator as claimed in claim 1 in which the inner conductor (7) is axially aligned with the waveguide (1).
3. A microwave applicator as claimed in claim 1 or 2 in which the waveguide (1) is a circular waveguide.
4. A microwave applicator as claimed in any one of the preceding claims in which the distal end face (8) is substantially flat and normal to the axis of the waveguide (1).
5. A microwave applicator as claimed in any one of claims 1 to 3 in which the distal end face (8) is flat or slightly domed and centred on the axis of the waveguide (1).
6. A microwave applicator as claimed in any one of the preceding claims in which the distal end face (8) has a polymer coating (22).
7. A microwave applicator as claimed in any one of the preceding claims in which the length and diameter of the waveguide (1), the length of the inner conductor (7) within the waveguide, and the permittivity of the dielectric material (2) are selected so that at the designed operating frequency, the waveguide is in resonance.
8. A microwave applicator as claimed in any one of the preceding claims in which the waveguide (1) is adapted so that in operation, when the distal end face (8) is in contact with biological tissue to be treated, forwards transmission from the distal end face is enhanced by the relative phase of reflections from the distal end face (8) and the input (4) to the waveguide; and when the distal end face (8) is in air or gas,

reflections to the input (4) are enhanced by the relative phase of reflections from the distal end face (8) and the input (4) to the waveguide.

9. A microwave applicator comprising a waveguide (1), a coaxial electrical input (4) with an inner conductor (7) extending longitudinally within one end of the waveguide to launch microwaves in the TM_{01} mode that travel to the distal end (8) of the waveguide and are transmitted into biological tissue to be treated, a diaphragm (20) of low loss dielectric material being provided within the waveguide (1) so as to extend laterally of the waveguide to reflect the microwaves travelling along it, the longitudinal location of the diaphragm (20) being selected in relation to the ends of the waveguide (1) so that the phase of reflections from the diaphragm (20) and said ends serve to reduce or cancel rearward reflections in the coaxial input (4).
10. A microwave applicator as claimed in claim 9 in which the thickness of the diaphragm (20), and the permittivity of the dielectric material from which it is made are selected to determine the magnitude of the rearward reflection of microwaves from the diaphragm (20) for optimum cancellation of the rearward reflection in the coaxial input.
11. A microwave applicator as claimed in claim 9 or 10 which is air-filled.
12. A microwave applicator as claimed in any one of the preceding claims in which the waveguide launches microwaves in the TM_{01} mode.
13. A method of heat treating surface tissue using the microwave applicator of any one of claims 1 to 12 in which the end face (8) of the waveguide (1) is brought into contact with the surface tissue.
14. A method as claimed in claim 13 in which the surface tissue is internal tissue and the applicator is inserted into a body for treatment.
15. A method as claimed in claim 14 in which the insertion of the applicator is via a Trocar.

16. A method as claimed in claim 13 in which the surface tissue is the external skin of the body.
17. A method of treating a liver in a body comprising providing a microwave applicator having a treatment head at one end capable of emitting microwave radiation from an emitting face, inserting the microwave applicator through an incision into the body positioning the head of the microwave applicator in contact with a surface of the liver with the emitting face adjacent to a region to be treated, and powering the microwave applicator so that the emitting face emits microwave radiation that heats said region to be treated.
18. A method of treating biological tissue to stop bleeding comprising providing a microwave applicator having a treatment head at one end capable of emitting microwave radiation from an emitting face, positioning the head of the microwave applicator in contact with a surface of the biological tissue to be treated with the emitting face adjacent to bleeding tissue to be treated, and powering the microwave applicator so that the emitting face emits radiation that heats the bleeding tissue to be treated.
19. A method of treating a skin condition such as psoriasis using a microwave applicator having a microwave emitting window which is brought into contact with, or into close proximity of, skin to be treated and is powered so as to emit microwave radiation and irradiate the skin to be treated.

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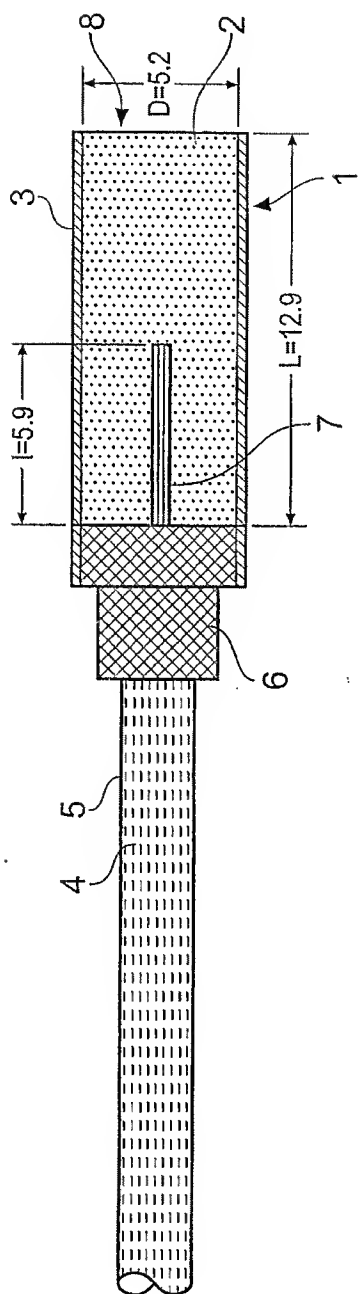


Fig. 1

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S11 FORWARD REFLECTION

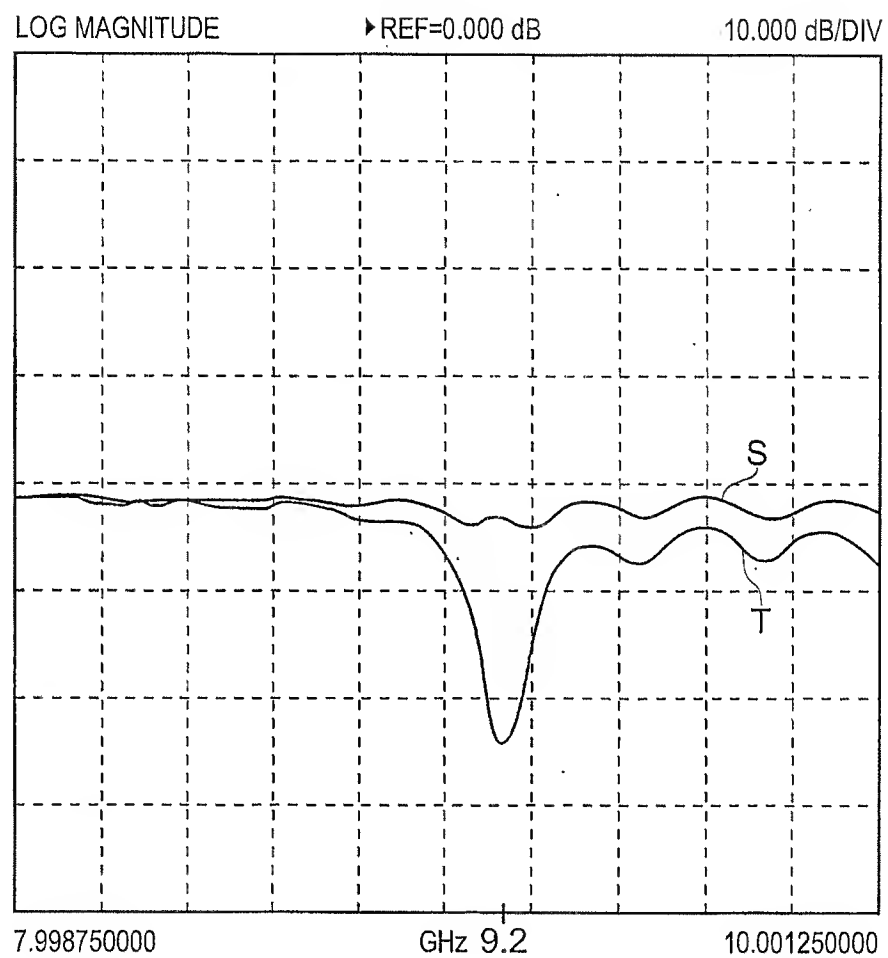


Fig. 2

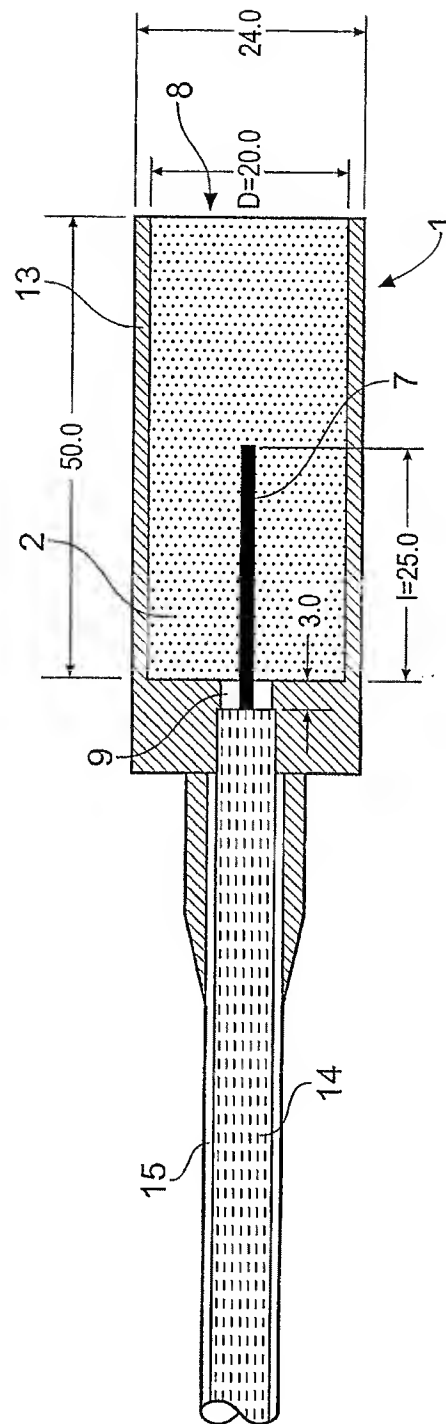


Fig. 3

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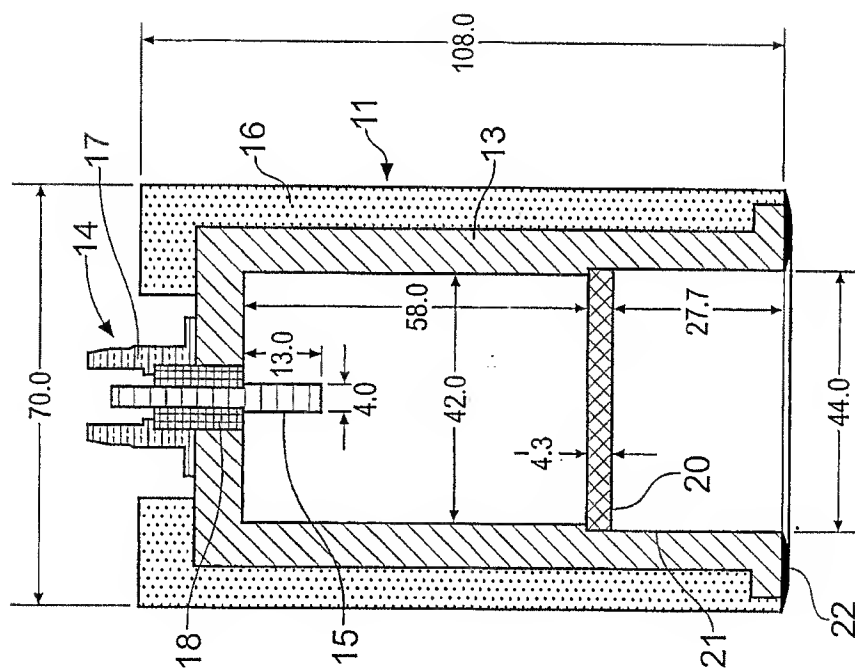


Fig. 4

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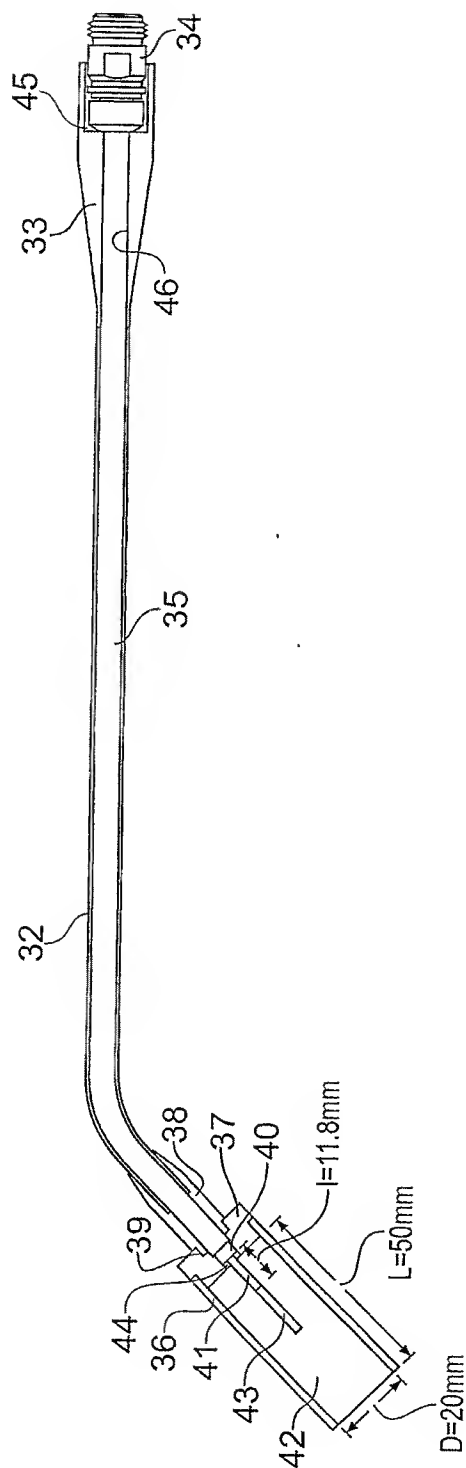


Fig. 5

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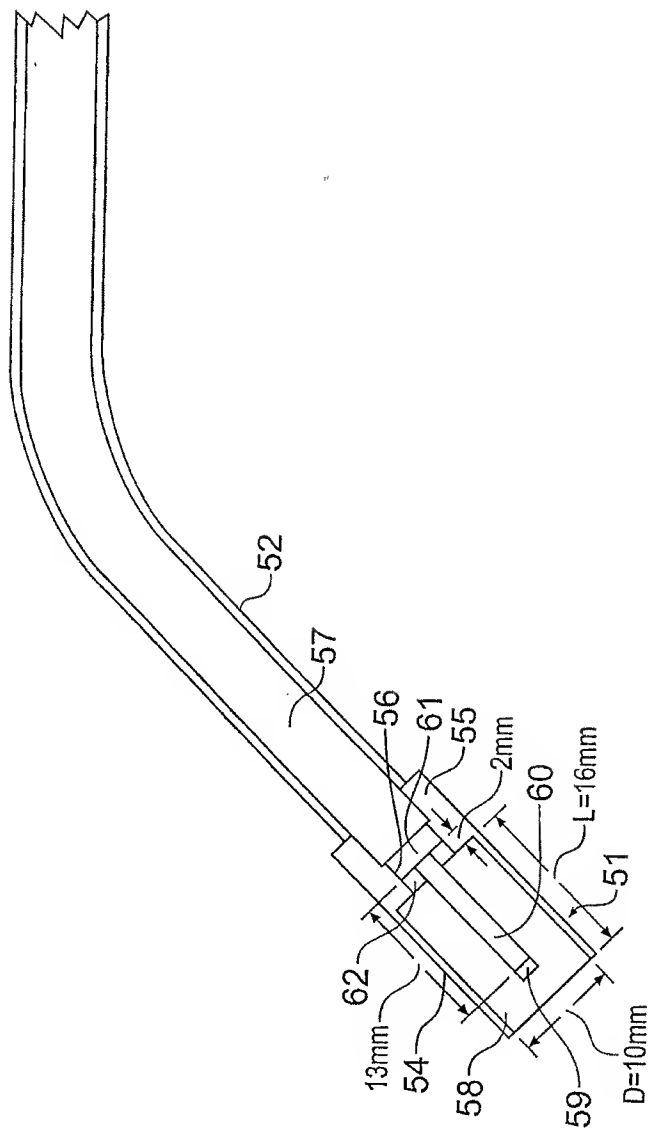


Fig. 6

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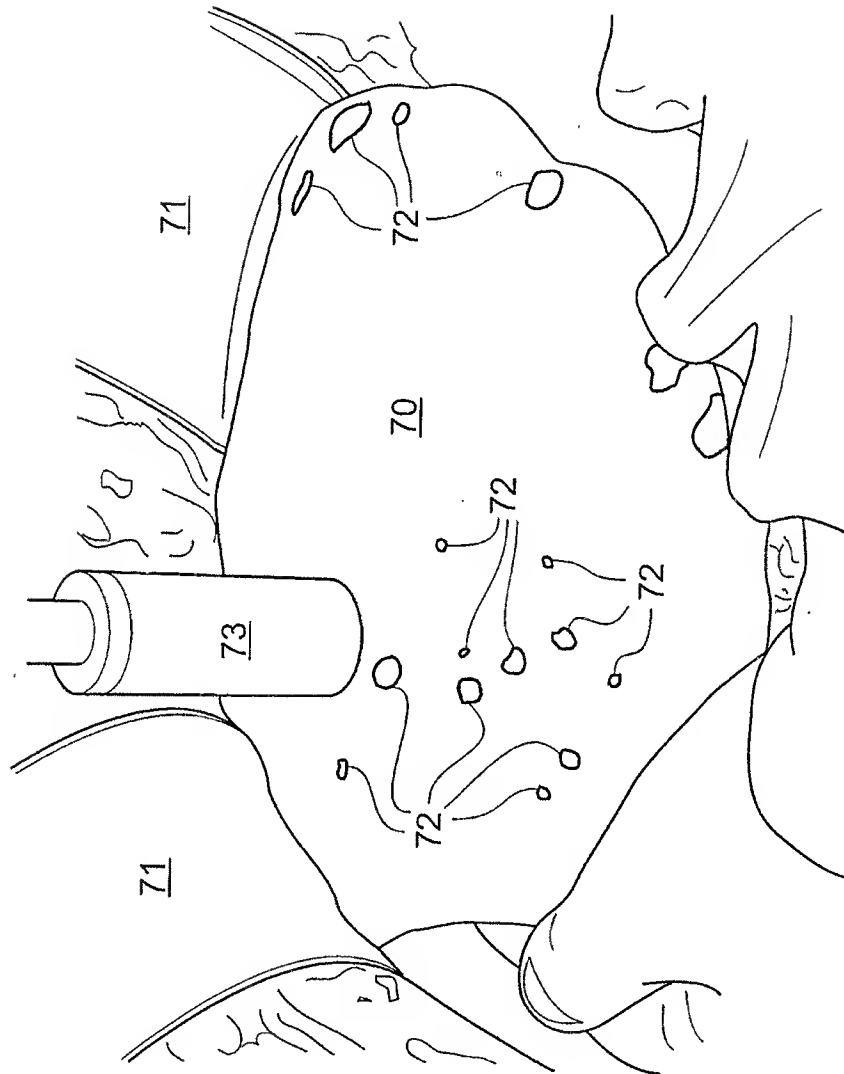


Fig. 7

INTERNATIONAL SEARCH REPORT

PCT/GB 03/04082

A. CLASSIFICATION OF SUBJECT MATTER
IPC 7 A61N5/04

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 7 A61N

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the International search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 4 446 874 A (VAGUINE VICTOR A) 8 May 1984 (1984-05-08)	1,3-8
Y	column 4, line 42 -column 8, line 61; figures 2,4	2
Y	US 3 065 752 A (FRITZ POTZL) 27 November 1962 (1962-11-27)	2
	column 2, line 10 - line 46; figure 1A	
A	EP 0 073 709 A (CENTRE NAT RECH SCIENT) 9 March 1983 (1983-03-09)	1-12
	page 2, line 27 -page 4, line 22	
A	EP 0 294 854 A (UNIV GLASGOW) 14 December 1988 (1988-12-14)	1-9,12
	column 7, line 10 -column 8, line 14; figures 6-8	
	-/--	

☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

* Special categories of cited documents:

- *A* document defining the general state of the art which is not considered to be of particular relevance
- *E* earlier document but published on or after the international filing date
- *L* document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- *O* document referring to an oral disclosure, use, exhibition or other means
- *P* document published prior to the international filing date but later than the priority date claimed

- *T* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
- *X* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
- *Y* document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.
- *Z* document member of the same patent family

Date of the actual completion of the international search

23 January 2004

Date of mailing of the international search report

02/02/2004

Name and mailing address of the ISA

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Artikis, T

INTERNATIONAL SEARCH REPORT

PCT/GB 03/04082

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 4 891 483 A (KIKUCHI MAKOTO ET AL) 2 January 1990 (1990-01-02) column 3, line 22 -column 4, line 47; figure 5 -----	1,9

INTERNATIONAL SEARCH REPORT

PCT/GB 03/04082

Box I Observations where certain claims were found unsearchable (Continuation of item 1 of first sheet)

This International Search Report has not been established in respect of certain claims under Article 17(2)(a) for the following reasons:

1. ☒ Claims Nos.: 13-19
because they relate to subject matter not required to be searched by this Authority, namely:
Rule 39.1(iv) PCT - Method for treatment of the human or animal body by therapy
2. ☐ Claims Nos.:
because they relate to parts of the International Application that do not comply with the prescribed requirements to such an extent that no meaningful International Search can be carried out, specifically:
3. ☐ Claims Nos.:
because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a).

Box II Observations where unity of invention is lacking (Continuation of item 2 of first sheet)

This International Searching Authority found multiple inventions in this International application, as follows:

1. ☐ As all required additional search fees were timely paid by the applicant, this International Search Report covers all searchable claims.
2. ☐ As all searchable claims could be searched without effort justifying an additional fee, this Authority did not invite payment of any additional fee.
3. ☐ As only some of the required additional search fees were timely paid by the applicant, this International Search Report covers only those claims for which fees were paid, specifically claims Nos.:
4. ☐ No required additional search fees were timely paid by the applicant. Consequently, this International Search Report is restricted to the invention first mentioned in the claims; it is covered by claims Nos.:

Remark on Protest

- ☐ The additional search fees were accompanied by the applicant's protest.
- ☐ No protest accompanied the payment of additional search fees.

INTERNATIONAL SEARCH REPORT

PCT/GB 03/04082

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